

# KOMMUNIKÁCIÓ 2X2-ES MIMO FELHASZNÁLÁSÁVAL

Ladvánszky János

HTE előadás

2022. 02. 09

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# OUTLINE

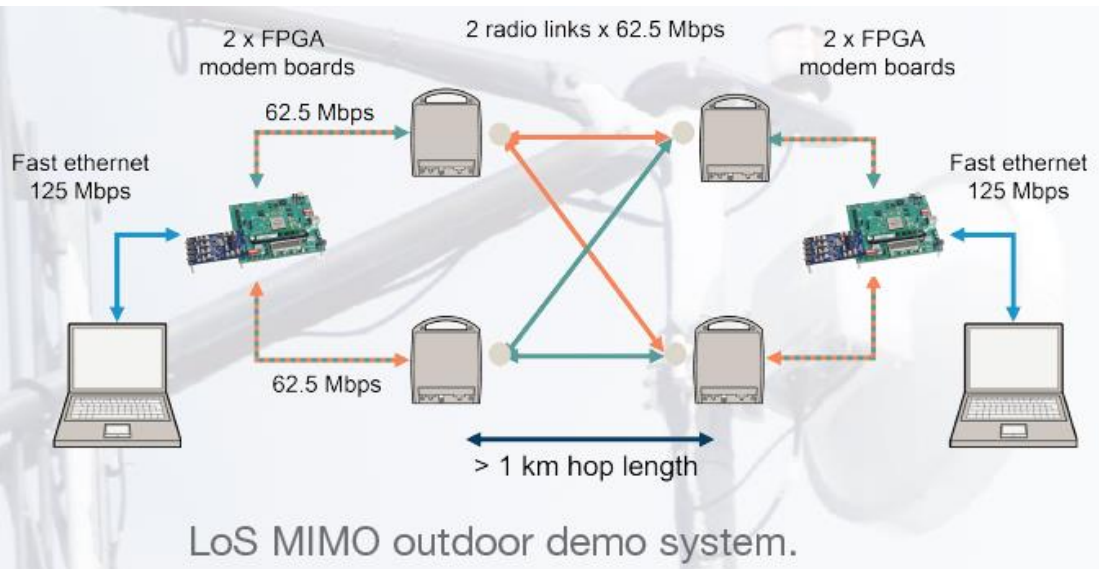
## › 2x2 LoS MIMO model

- reference transmission model
- receiver analytical description
- SIMULINK receiver model summary
- FPGA implementation considerations and results
- false detection cancellation method

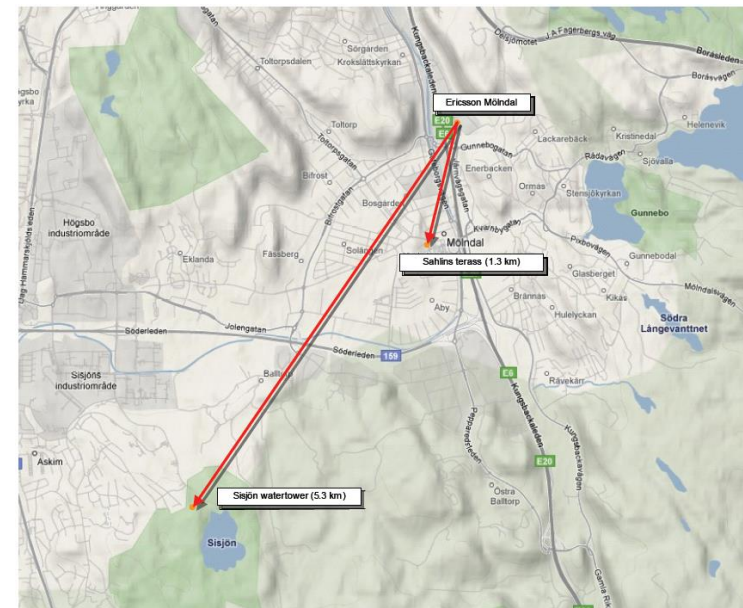
# PROJECT GOALS

## › Demonstrate 2x2 MIMO transmission

- develop and implement receiver algorithms in FPGA
- demonstration on laboratory setup
- demonstrate on outdoor link



*31.25 MS/s, QPSK transmission*  
*125 MHz ADC, 250 MHz FPGA clock*  
*Altera Stratix III evaluation board*



The two test links in Gothenburg.

# PARTICIPANTS

ANNA RHODIN – ERICSSON  
GOTHENBURG – MEASUREMENTS

GÁBOR KOVÁCS – ETH – INPUT  
SIMULATOR

GÉZA BALÁZS – ETH- FPGA

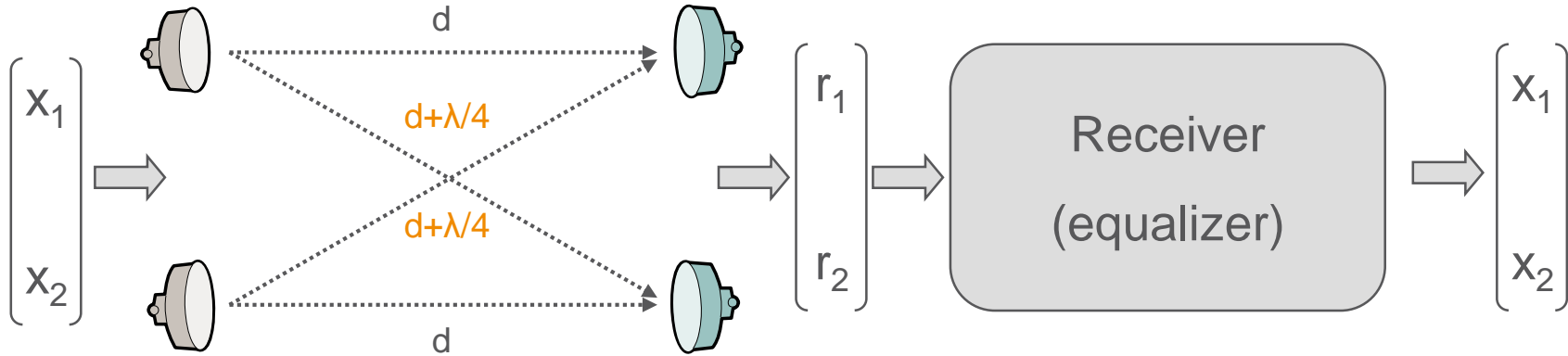
JÁNOS LADVÁNSZKY – ETH –  
ALGORITHM OF RECEPTION

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# CONCEPT OF MIMO RADIOS



2x2 MIMO microwave link  
(Line-of-Sight)

$$\underline{r} = \begin{pmatrix} 1 & \exp\left(-j\frac{\pi}{2}\right) \\ \exp\left(-j\frac{\pi}{2}\right) & 1 \end{pmatrix} \cdot \underline{x}$$

$$\hat{\underline{x}} = \frac{1}{2} \cdot \begin{pmatrix} 1 & e^{j\frac{\pi}{2}} \\ e^{j\frac{\pi}{2}} & 1 \end{pmatrix} \cdot \underline{r}$$

$\frac{\pi}{2} \Rightarrow \varphi(t)$  adaptive equalizer is needed!

- > MCMA has been chosen for its simplicity and robustness

# EQUALIZER OVERVIEW

Choose as simple as possible: MCMA algorithm

MCMA is capable of fixing the real and imaginary parts in the constellation

For one channel:  $\hat{x}(k+1) = \underline{w}^{*T}(k) \underline{r}$

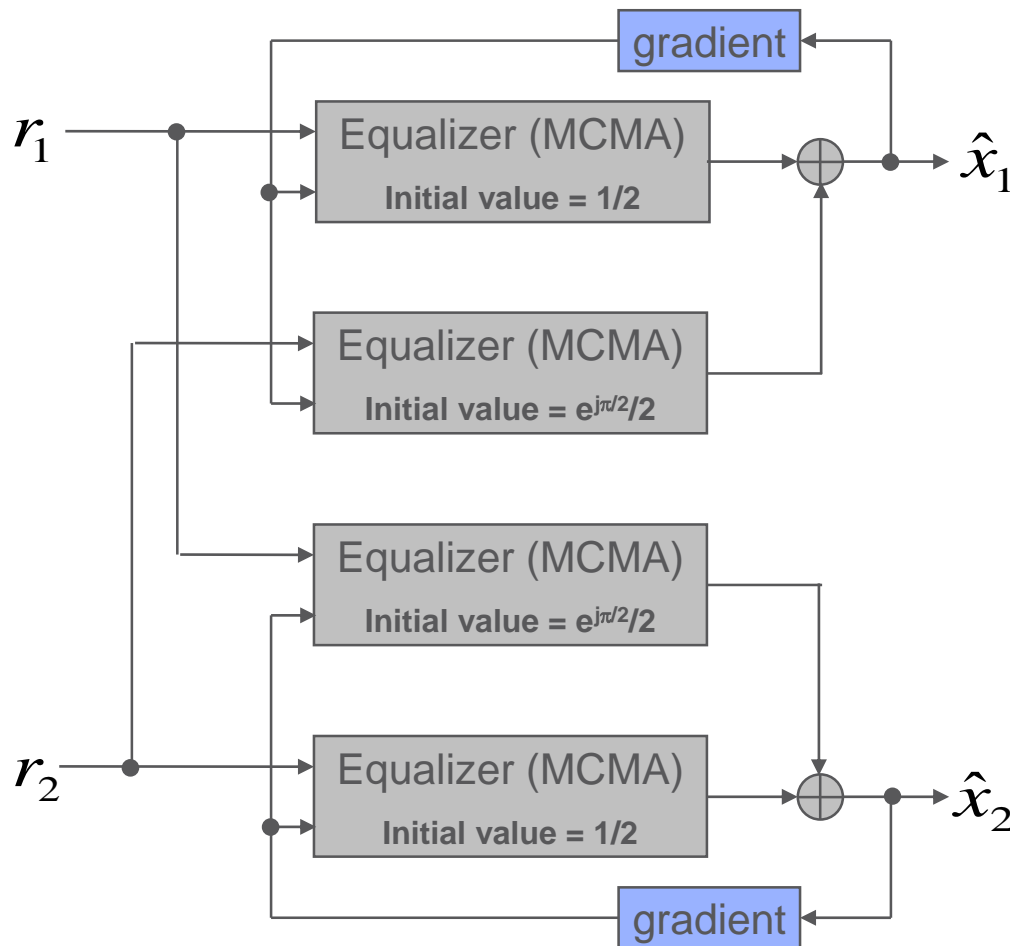
Weight update:  $\underline{w}(k+1) = \underline{w}(k) - \mu_1 \text{Re}(\hat{x}(k))(\text{Re}(\hat{x}(k))^2 - R_{\text{Re}}) \underline{r} +$   
 $+ j\mu_2 \text{Im}(\hat{x}(k))(\text{Im}(\hat{x}(k))^2 - R_{\text{Im}}) \underline{r}$

MCMA radii:

$$R_{\text{Re}} = \frac{E[\text{Re}(\hat{x})^4]}{E[\text{Re}(\hat{x})^2]} \quad R_{\text{Im}} = \frac{E[\text{Im}(\hat{x})^4]}{E[\text{Im}(\hat{x})^2]}$$

# EQUALIZER STRUCTURE

› MCMA equalizer in each path:

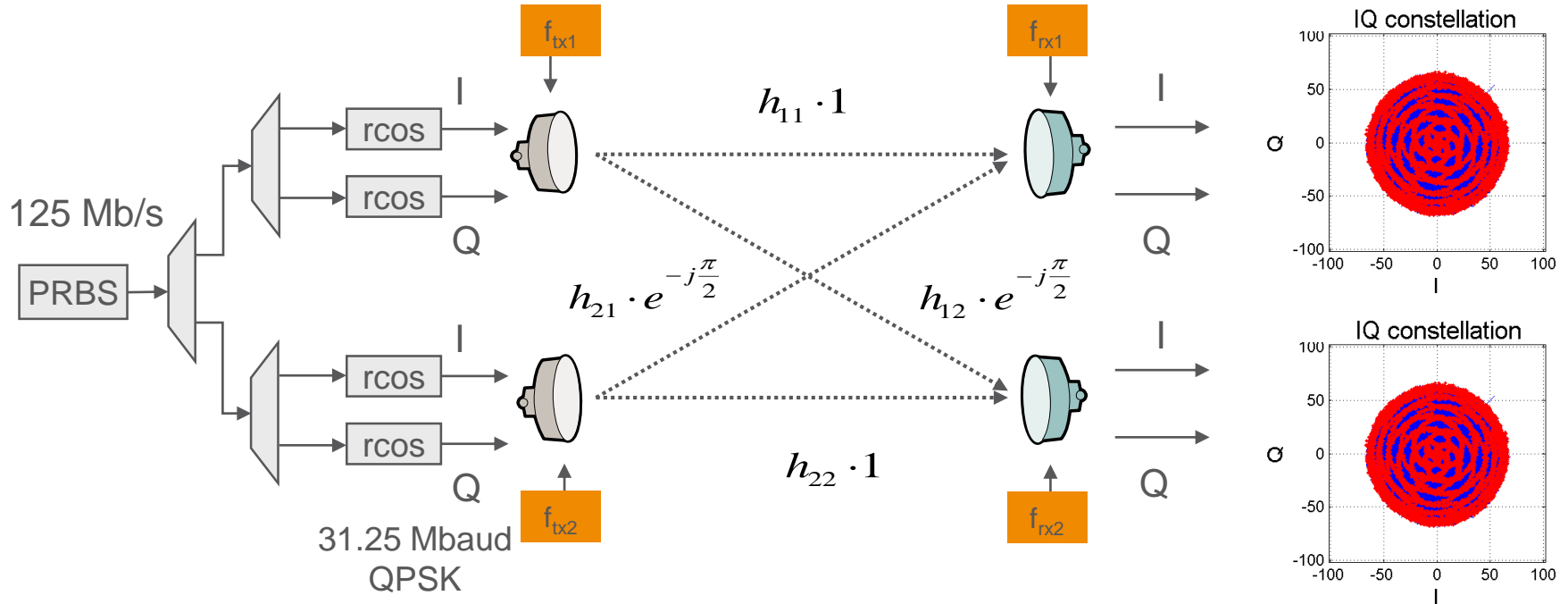


- 10 tap equalizer filter  
(125 MHz / 25MS/s =  
= 5 sample / symbol)
- Initial values *in the first tap*
  - ›  $1/2$  in the direct path
  - ›  $1/2j$  in the cross-path
- conjugate gradient is fed  
back from appropriate output



# PRACTICAL TRANSMISSION MODEL

## › Practical imperfections:



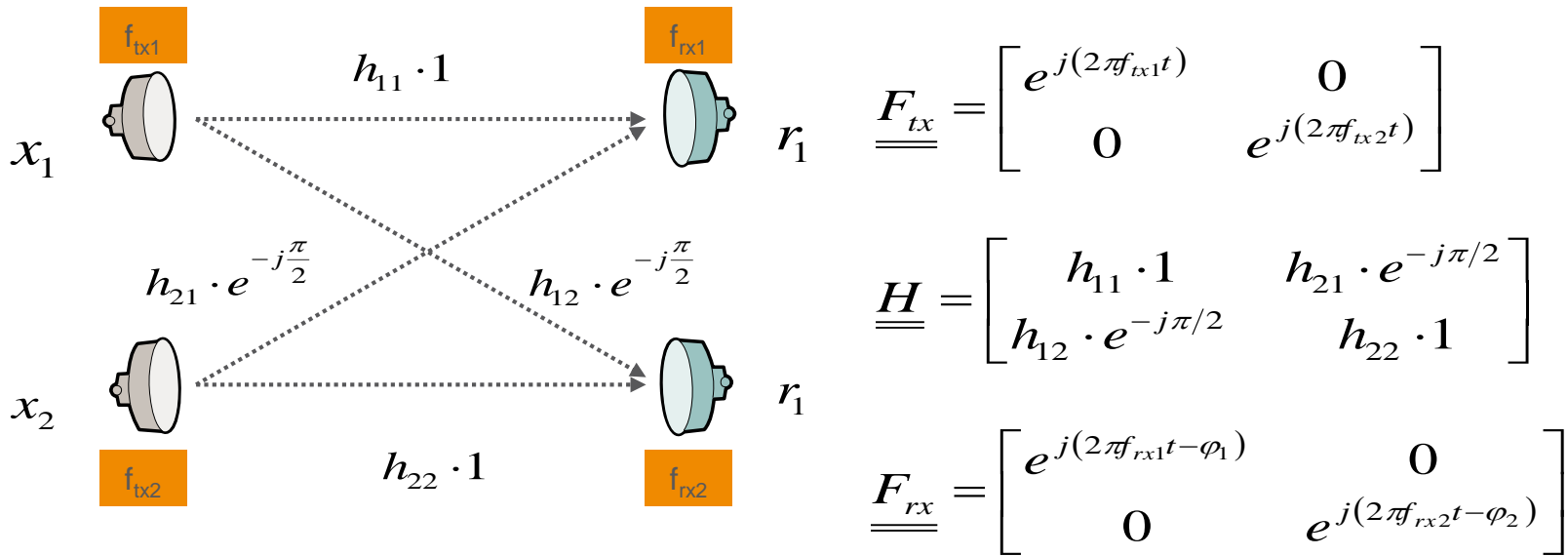
$$\underline{r} = \left[ \underline{F}_{Rx} \cdot \underline{H} \cdot \underline{F}_{Tx} \right] \cdot \underline{x} + \underline{N}$$

Receivers frequency deviation

LoS MIMO channel

Transmitters frequency deviation

# ANALYTICAL DESCRIPTION



$f_{tx1}$ ,  $f_{tx2}$ ,  $f_{rx1}$ ,  $f_{rx2}$  – difference from nominal frequency values

$h_{11}$ ,  $h_{12}$ ,  $h_{21}$ ,  $h_{22}$  – antenna gain differences + time dependent channel transfer functions

$\varphi_1$ ,  $\varphi_2$  – random phase of receiver oscillator

› Note: multiplication operator is not exact: convolution operator should be used, as  $h_{xx}$  is the time-domain equivalent of the radio channel. However, convolution would also not be precise in the equations because multiplication by a non-constant in time is not a linear operator.

# TEST WAVEFORM GENERATION (1)

› Basis for understanding LoS MIMO channels and to provide test signals for receivers:

– adjustable parameters (can be time dependent):

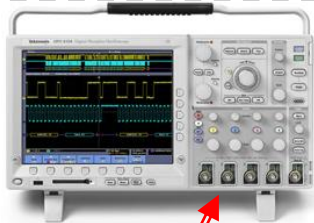
- ›  $f_{tx1}, f_{tx2}, f_{rx1}, f_{rx2}$  – frequency difference from nominal
- ›  $\phi_{12}, \phi_{21}$  – cross-channel phase difference (eg. mast swing)
- › symbol rate (*25 MHz in measured data*)
- › sampling rate (125 MHz)
- › AWGN level

– Implemented functionalities:

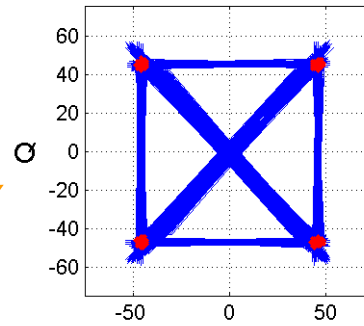
- › random input bit stream (PRBS) with RRCOS filter for QPSK
- › time dependent transmitter & receiver frequency matrices
- › time dependent MIMO channel matrix (only complex coefficient, no radio channel modelling)

# TEST WAVEFORM GENERATION (2)

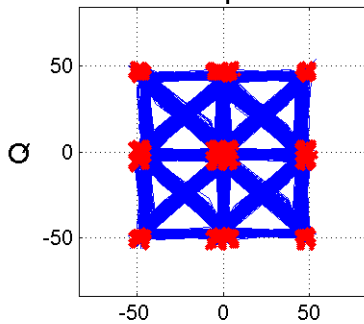
## › Test waveform generators:



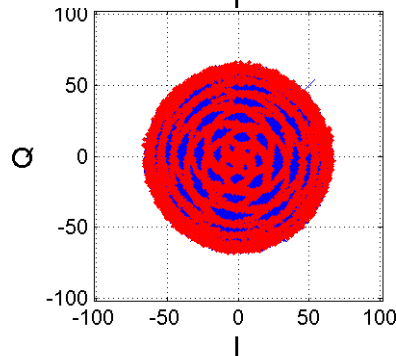
*Altera Stratix III  
development board +  
+ DAC/ADC extension cards*



- output constellation
  - › only one source
  - › no channel
  - › no rotation



- output constellation
  - › both source transmit
  - › channel enabled
  - › no rotation



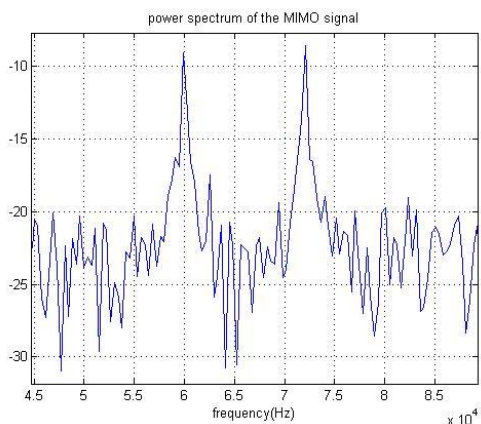
- output constellation
  - › both source transmit
  - › channel enabled
  - › both transmitters and receivers enabled

*Measured at FPGA output*

# SIMULATION EXAMPLE

> How to compensate for the frequency deviations?

- Problem:  $f_{tx1}, f_{tx2}, f_{rx1}, f_{rx2}$  are not explicitly present in the received signal:



$$f_{tx1} = 3kHz; f_{tx2} = 6kHz;$$

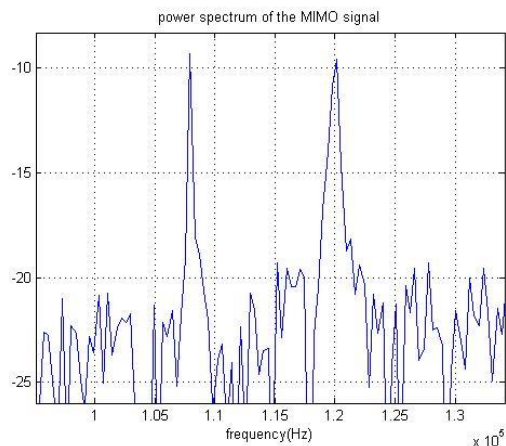
$$f_{rx1} = 12kHz; f_{rx2} = 24kHz$$

$$(f_{tx1} + f_{rx1}) \cdot 4 = 60kHz$$

$$(f_{tx2} + f_{rx1}) \cdot 4 = 72kHz$$

$$(f_{tx1} + f_{rx2}) \cdot 4 = 108kHz$$

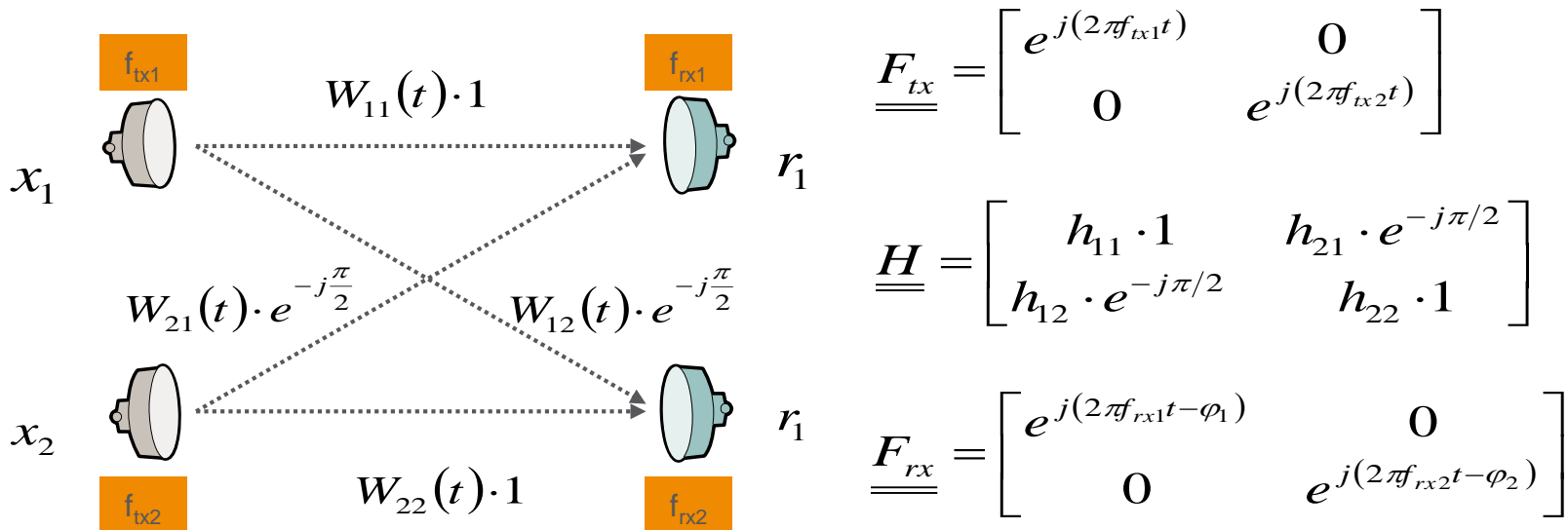
$$(f_{tx2} + f_{rx2}) \cdot 4 = 120kHz$$



**In the spectra the frequencies appear combined, and not separately as they are needed in the synchronization**

# ANALYTICAL DESCRIPTION

› These frequency combinations can also be derived analytically



$$\underline{r} = \left[ \underline{\underline{F}}_{Rx} \cdot \underline{\underline{H}} \cdot \underline{\underline{F}}_{Tx} \right] \cdot \underline{x} + \underline{N}$$

$$r_1 = h_{11} \cdot 1 \cdot e^{j(2\pi(f_{tx1} + f_{rx1})t - \varphi_1)} \cdot x_1 + h_{21} \cdot e^{-j\pi/2} \cdot e^{j(2\pi(f_{tx2} + f_{rx1})t - \varphi_1)} \cdot x_2$$

$$r_2 = h_{12} \cdot e^{-j\pi/2} \cdot e^{j(2\pi(f_{tx1} + f_{rx2})t - \varphi_2)} \cdot x_1 + h_{22} \cdot 1 \cdot e^{j(2\pi(f_{tx2} + f_{rx2})t - \varphi_2)} \cdot x_2$$

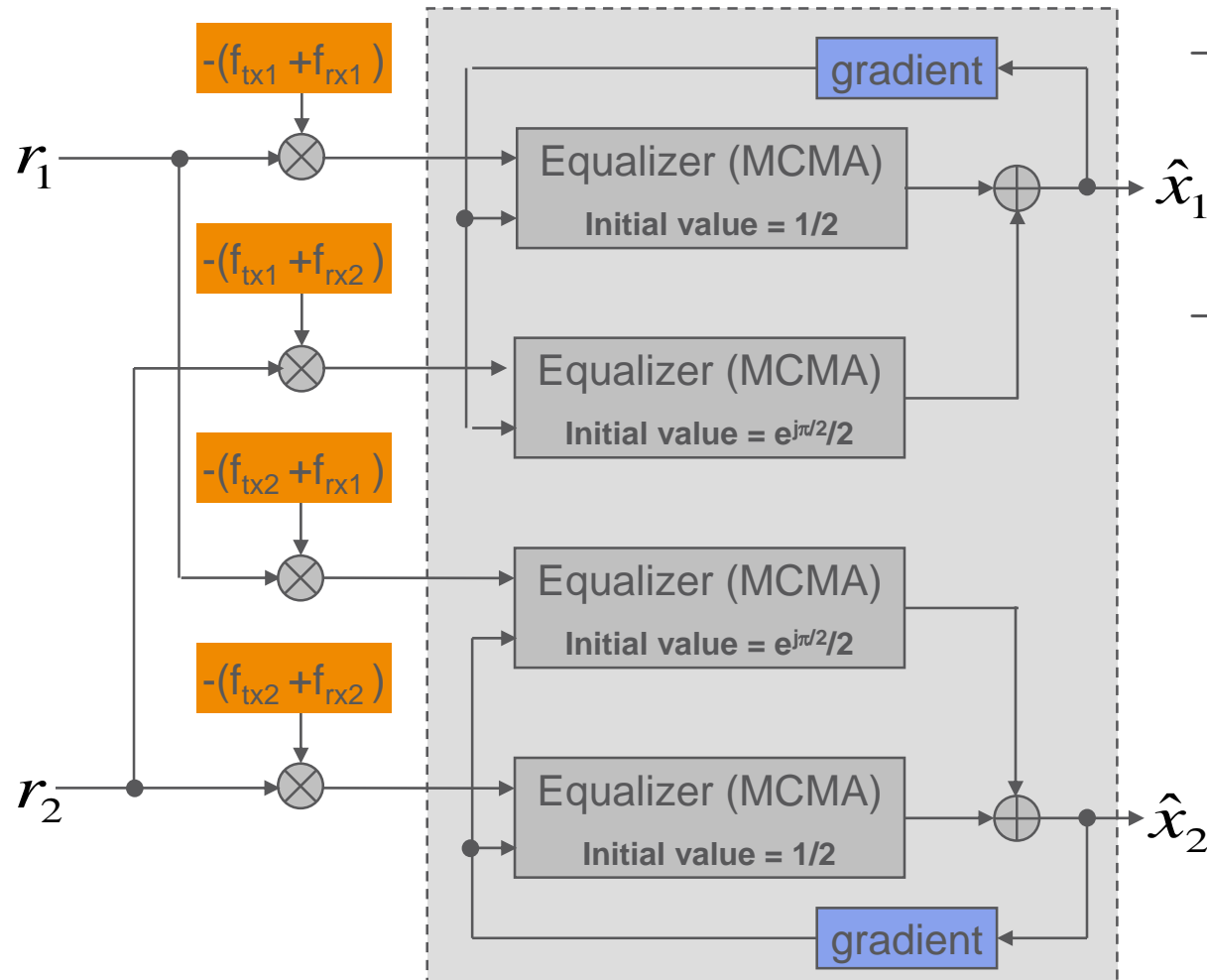
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# RECEIVER STRUCTURE (1)

- › Frequency compensations and equalization architecture:



- First stage compensates for the frequency rotations:
  - › Tx1 in upper pair
  - › Tx2 in lower pair
- Second stage equalizes MIMO radio channel effect as described earlier.

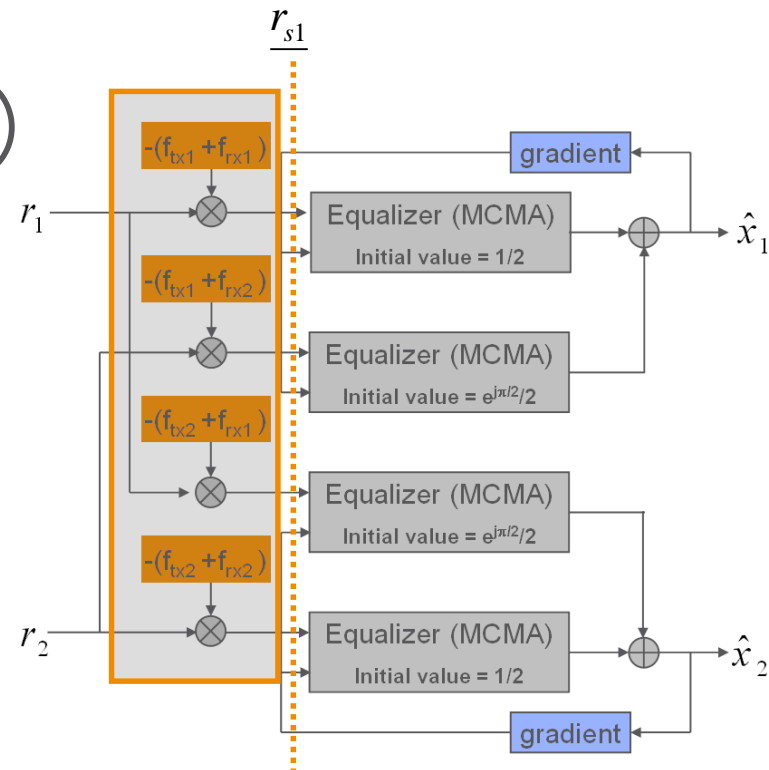
## Major advantage:

**All rotation cancelled,**  
though equalizers  
(*theoretically*) do not need to  
compensate for any  
constellation rotation!



# RECEIVER STRUCTURE (2)

- › Matrix description of the first stage:
  - Tx1 rotation is compensated in upper left corner
  - Tx2 rotation is compensated in lower right corner



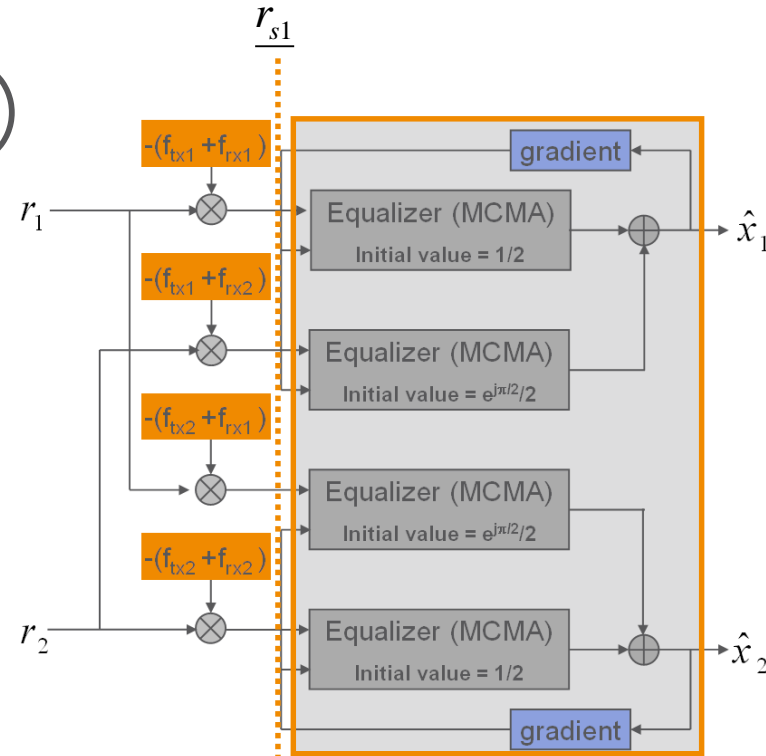
$$\underline{r}_{s1} = \begin{bmatrix} e^{-j2\pi(f_{tx1}+f_{rx1})t} & 0 \\ 0 & e^{-j2\pi(f_{tx1}+f_{rx2})t} \\ e^{-j2\pi(f_{tx2}+f_{rx1})t} & 0 \\ 0 & e^{-j2\pi(f_{tx2}+f_{rx2})t} \end{bmatrix} \begin{bmatrix} h_{11} \cdot e^{-j\varphi_1} \cdot e^{j2\pi(f_{tx1}+f_{rx1})t} & h_{21} \cdot e^{-j\varphi_2} \cdot e^{-j\frac{\pi}{2}} \cdot e^{j2\pi(f_{tx2}+f_{rx1})t} \\ h_{12} \cdot e^{-j\varphi_1} \cdot e^{-j\frac{\pi}{2}} \cdot e^{j2\pi(f_{tx1}+f_{rx2})t} & h_{22} \cdot e^{-j\varphi_2} \cdot e^{j2\pi(f_{tx2}+f_{rx2})t} \end{bmatrix} \underline{x} =$$

$$= \begin{bmatrix} h_{11} \cdot e^{-j\varphi_1} & h_{21} \cdot e^{-j\varphi_2} \cdot e^{-j\frac{\pi}{2}} \cdot e^{j2\pi(f_{tx2}-f_{tx1})t} \\ h_{12} \cdot e^{-j\varphi_1} \cdot e^{-j\frac{\pi}{2}} & h_{22} \cdot e^{-j\varphi_2} \cdot e^{j2\pi(f_{tx2}-f_{tx1})t} \\ h_{11} \cdot e^{-j\varphi_1} \cdot e^{j2\pi(f_{tx1}-f_{tx2})t} & h_{21} \cdot e^{-j\varphi_2} \cdot e^{-j\frac{\pi}{2}} \\ h_{12} \cdot e^{-j\varphi_1} \cdot e^{-j\frac{\pi}{2}} \cdot e^{j2\pi(f_{tx1}-f_{tx2})t} & h_{22} \cdot e^{-j\varphi_2} \end{bmatrix} \underline{x}$$

# RECEIVER STRUCTURE (3)

› Matrix description of the second stage:

- equalizer need to compensate
  - › for different level of loss in MIMO channel paths
  - › random oscillator phases
  - › MIMO cross-path components
- no rotation compensation is required from the equalizer



$$\hat{\underline{x}} = \frac{1}{2} \begin{bmatrix} h_{11}^{-1} \cdot e^{j\varphi_1} & h_{12}^{-1} \cdot e^{j\varphi_1} \cdot e^{j\frac{\pi}{2}} & 0 & 0 \\ 0 & 0 & h_{21}^{-1} \cdot e^{j\varphi_2} \cdot e^{j\frac{\pi}{2}} & h_{22}^{-1} \cdot e^{j\varphi_2} \end{bmatrix} \begin{bmatrix} h_{11} \cdot e^{-j\varphi_1} \\ h_{12} \cdot e^{-j\varphi_1} \cdot e^{-j\frac{\pi}{2}} \\ h_{11} \cdot e^{-j\varphi_1} \cdot e^{j2\pi(f_{tx1}-f_{tx2})t} \\ h_{12} \cdot e^{-j\varphi_1} \cdot e^{-j\frac{\pi}{2}} \cdot e^{j2\pi(f_{tx1}-f_{tx2})t} \\ h_{21} \cdot e^{-j\varphi_2} \cdot e^{-j\frac{\pi}{2}} \cdot e^{j2\pi(f_{tx2}-f_{tx1})t} \\ h_{22} \cdot e^{-j\varphi_2} \cdot e^{j2\pi(f_{tx2}-f_{tx1})t} \\ h_{21} \cdot e^{-j\varphi_2} \cdot e^{-j\frac{\pi}{2}} \\ h_{22} \cdot e^{-j\varphi_2} \end{bmatrix} \underline{x} =$$

$$= \frac{1}{2} \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} \underline{x}$$

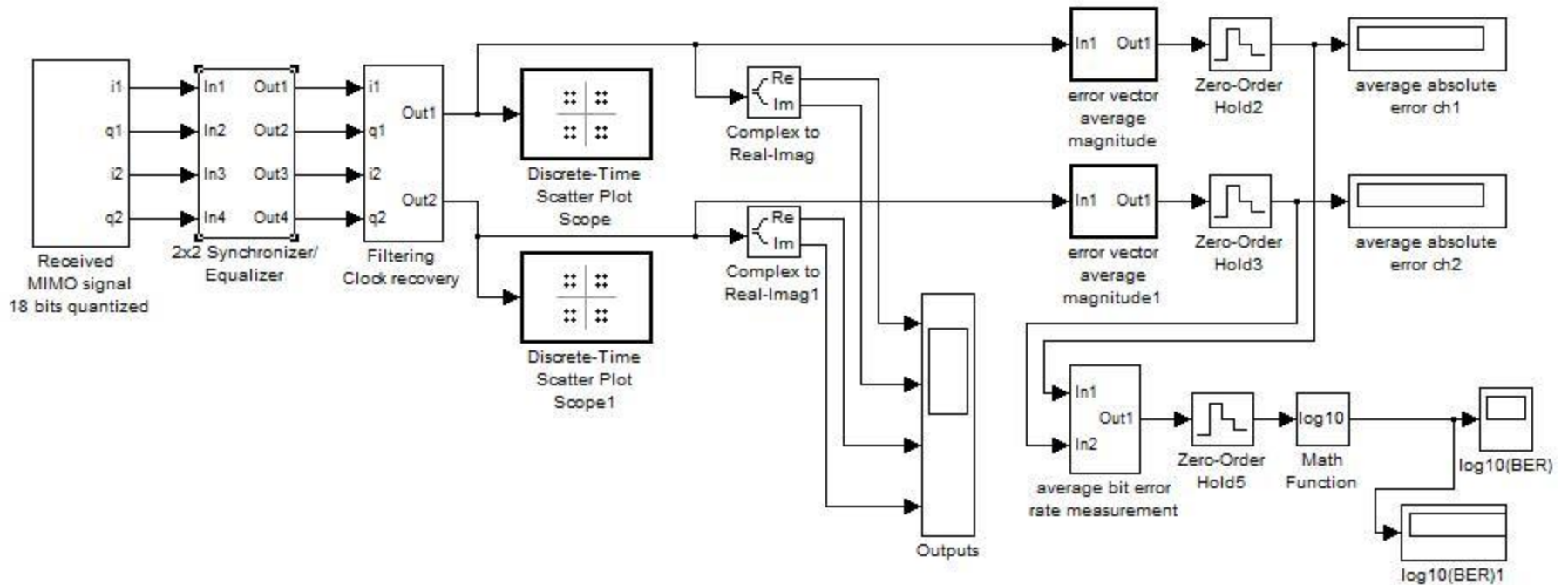
$$h_{11} \cdot h_{21} = h_{12} \cdot h_{22}$$

# OUTLINE

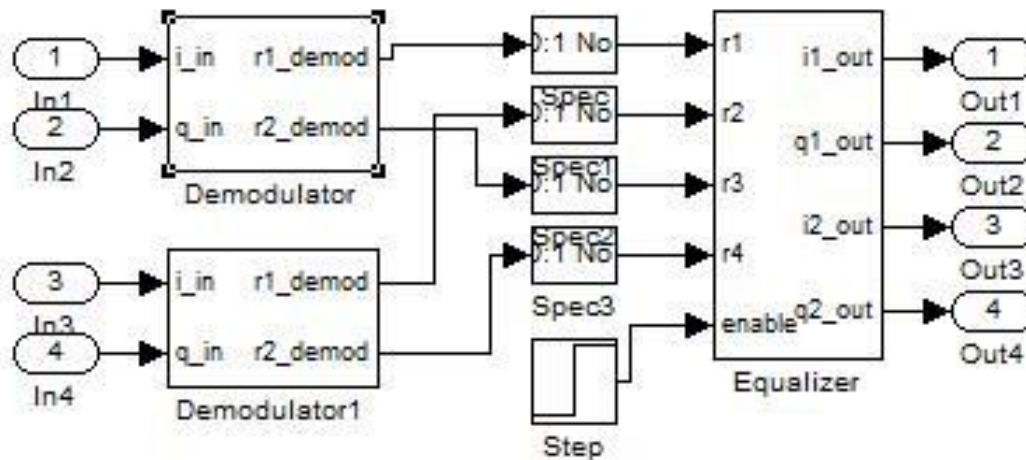
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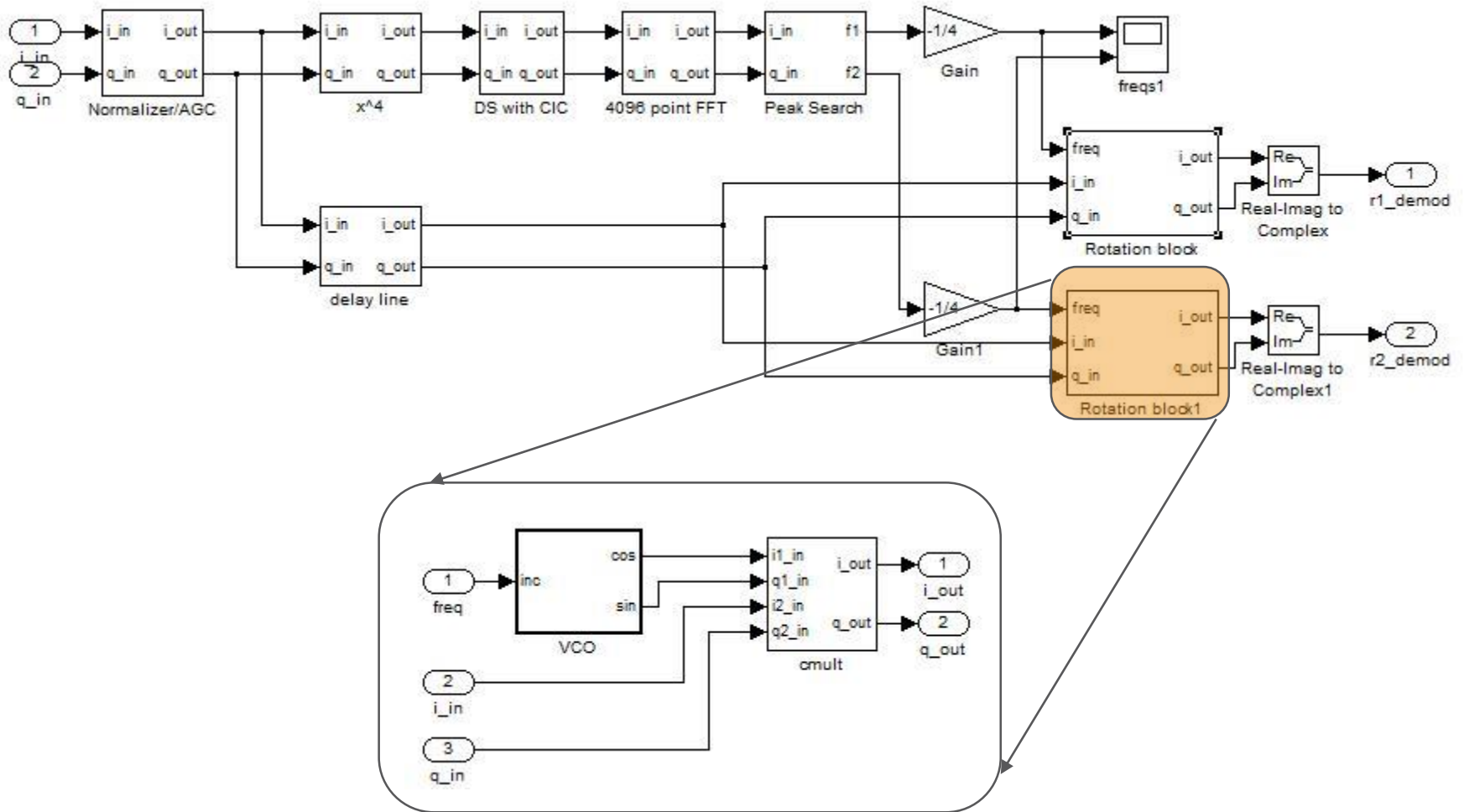
# SIMULINK SYSTEM DIAGRAM



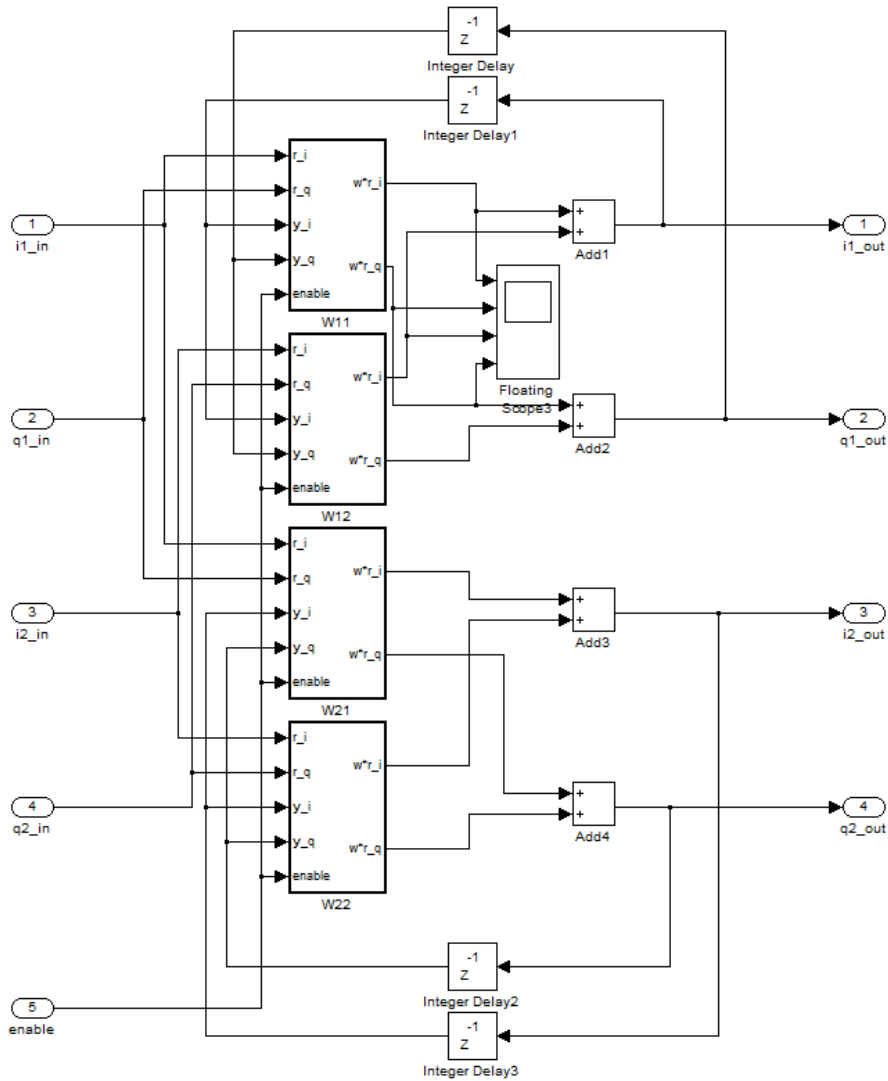
# SYNCHRONIZER/EQUALIZER



# DEMODULATOR AND ROTATOR

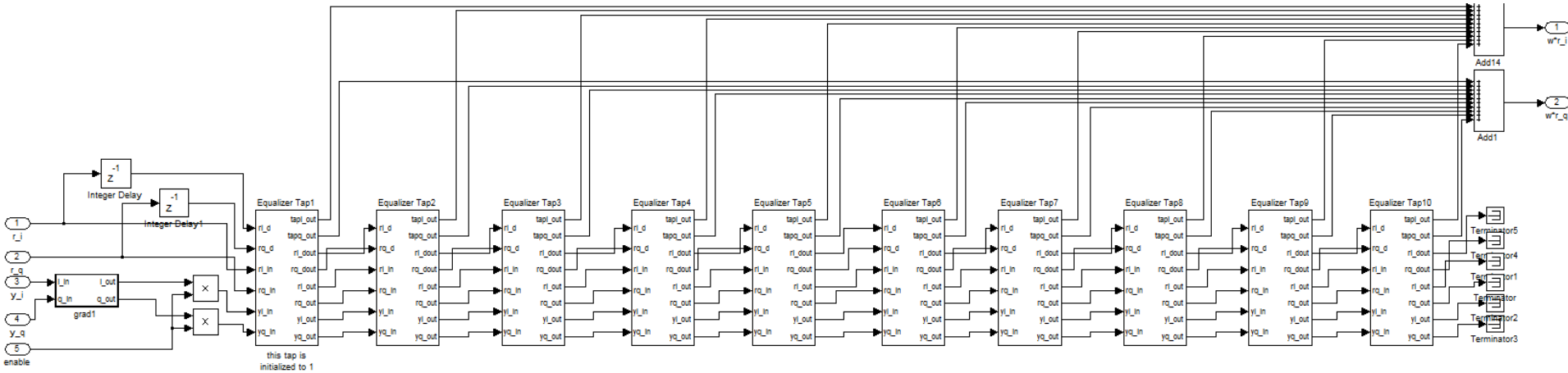


# EQUALIZER BLOCK DIAGRAM



- › Gradient block is placed in the equalizer module

# EQUALIZER MODULE



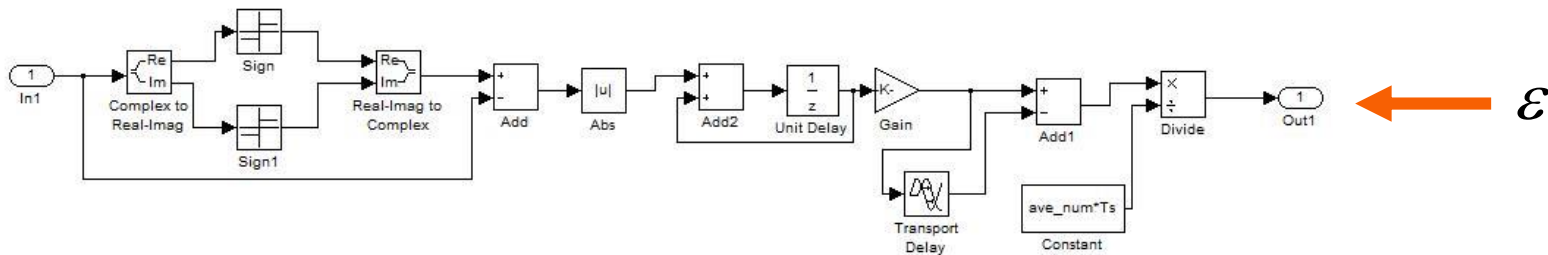


# QUANTITATIVE MEASURE OF RECEIVER ALGORITHM QUALITY

Average bit error rate as a function of time:  $BER = erfc(1/\varepsilon)$

where  $\varepsilon$  is the average deviation from the ideal constellation point that is obtained by sign() function

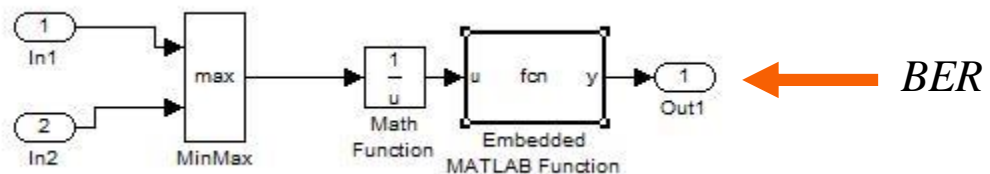
Condition: The erroneous constellation point is in the same quadrant as the error-free one



```

1 function y = fcn(u)
2 %#eml
3
4 y = erfc(u);

```



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# RECEIVED SIGNAL DECOMPOSITION

› Another analytical form of the received signal:

$$\begin{aligned} r_1 &= h_{11} \cdot e^{j(\varphi_{11} + 2\pi\Delta f_{11}t)} \cdot e^{j(2\pi(f_{tx1} + f_{rx1})t)} \cdot x_1 + h_{21} \cdot e^{j(\varphi_{12} + 2\pi\Delta f_{12}t)} \cdot e^{-j\pi/2} \cdot e^{j(2\pi(f_{tx2} + f_{rx1})t)} \cdot x_2 \\ r_2 &= h_{12} \cdot e^{j(\varphi_{21} + 2\pi\Delta f_{21}t)} \cdot e^{-j\pi/2} \cdot e^{j(2\pi(f_{tx1} + f_{rx2})t)} \cdot x_1 + h_{22} \cdot e^{j(\varphi_{22} + 2\pi\Delta f_{22}t)} \cdot e^{j(2\pi(f_{tx2} + f_{rx2})t)} \cdot x_2 \end{aligned}$$

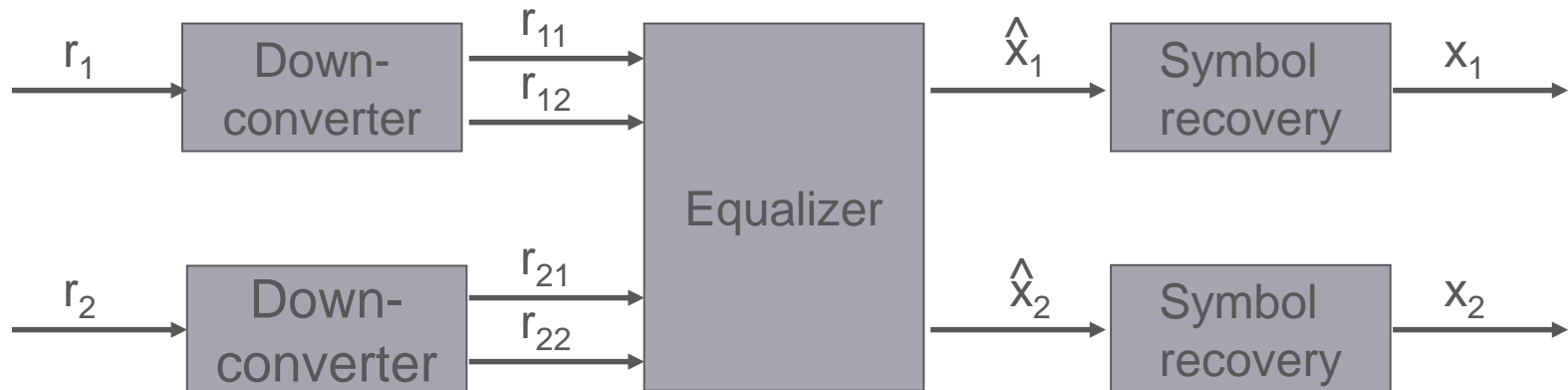
› Exact measurement of frequencies is not possible (discrete Fourier transform):

–  $\Delta f_{11}$ ,  $\Delta f_{12}$ ,  $\Delta f_{21}$ ,  $\Delta f_{22}$  – frequency measurement error

- Factors that change ‘slowly’ over time
- Factors that can change fast over time
- Factors that change very rapidly over time

# RECEIVER BLOCK DIAGRAM

- › Slow changes will be compensated by the equalizers
- › Moderate to fast changes will be compensated by the downconverter
- › The transmitted data stream is the fastest changing signal, its timing will be decoded, and the signal sampled by the timing recovery block



# OUTLINE

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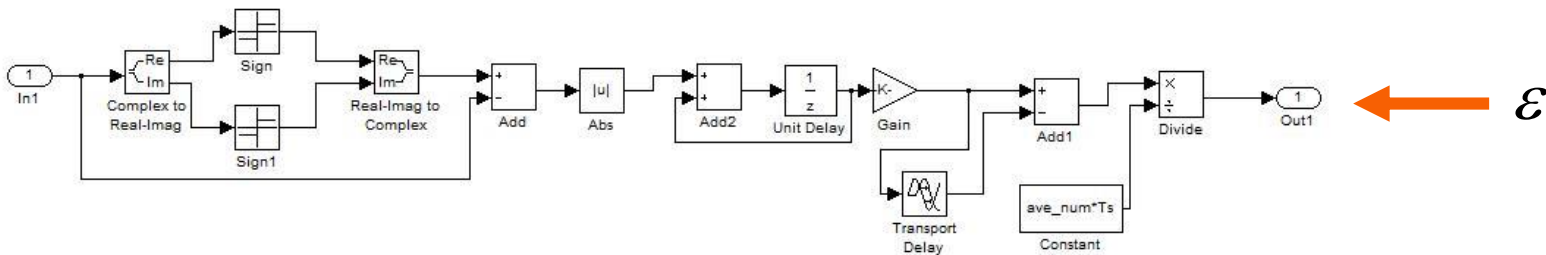
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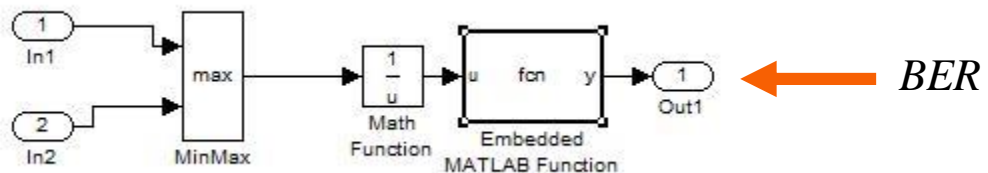
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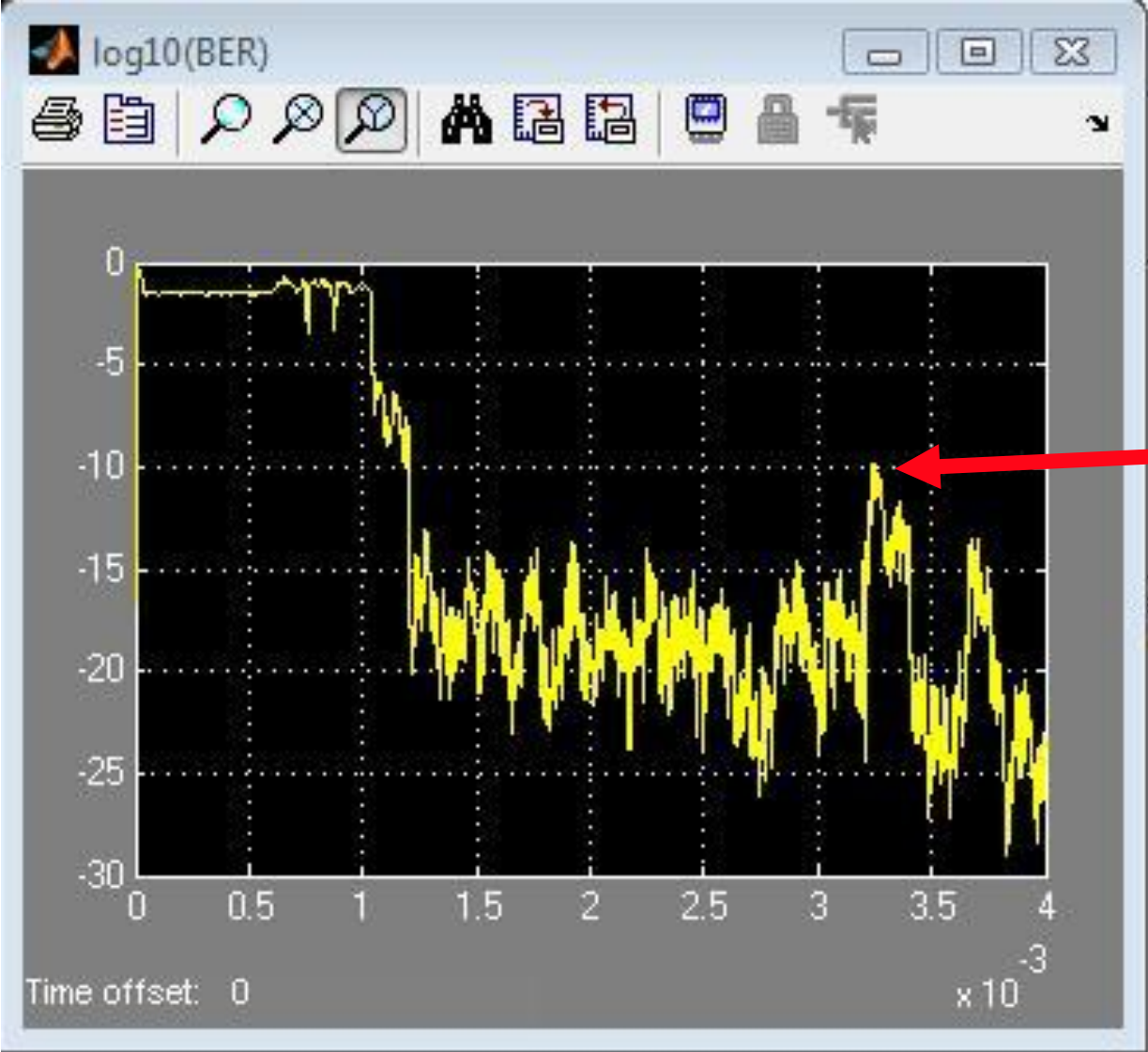
```

1 function y = fcn(u)
2 %#eml
3
4 y = erfc(u);

```



# BIT ERROR RATE



What is this?

# FALSE DETECTION CANCELLATION

Types of false detection

- Weaker form: i and q signals at the same channel exchange and one of them has opposite sign (no information loss)
- Stronger form: signals at different channels coincide (information loss)

Reason of false detection: Rotation of different equalizer coefficients without having a fixed angle difference between them

Appearance: Sudden increase in BER

Defense: Compensating rotations with fixed angle difference between different equalizer channels



# NEW CONCEPT OF FALSE DETECTION CANCELLATION

Restriction for rotation of weighting factors in neighbouring channels

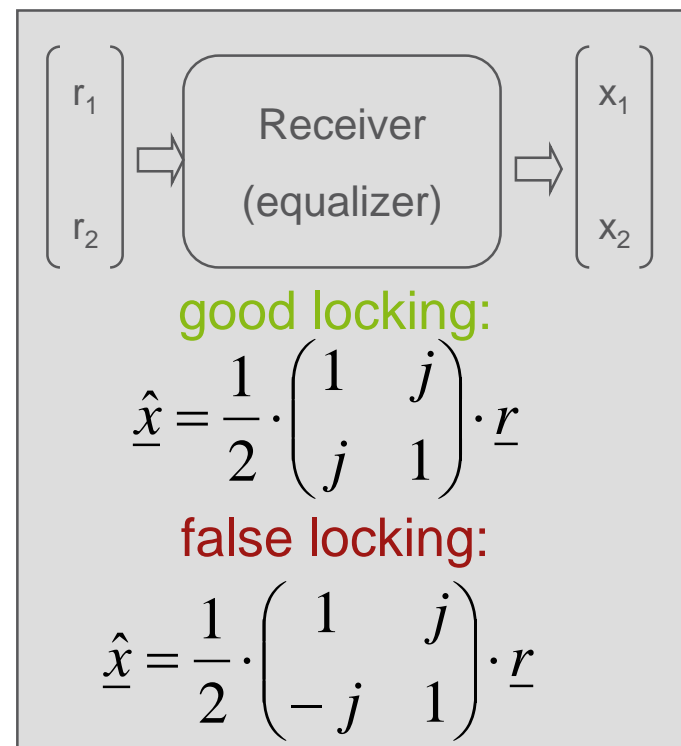
Ideal case:  $w_{11}=1, w_{12}=j$

Rotation is allowed with nearly  $90^\circ$  phase difference

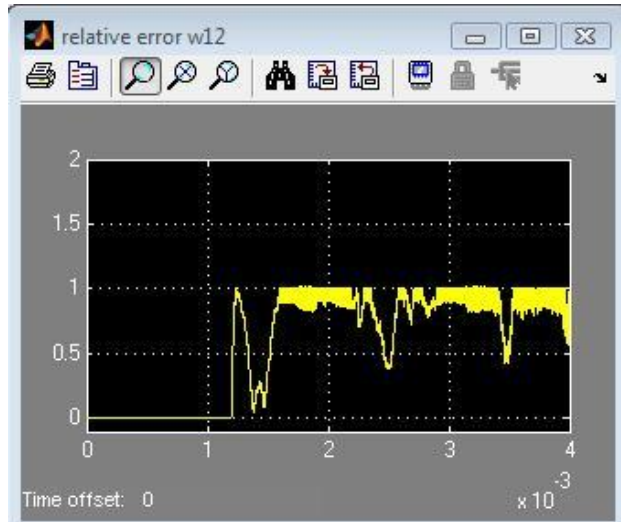
Detection of phase difference:  $\delta = \left| \frac{w_{12} - jw_{11}}{w_{12} + jw_{11}} \right| * 2$

Restriction:  $\delta < K$

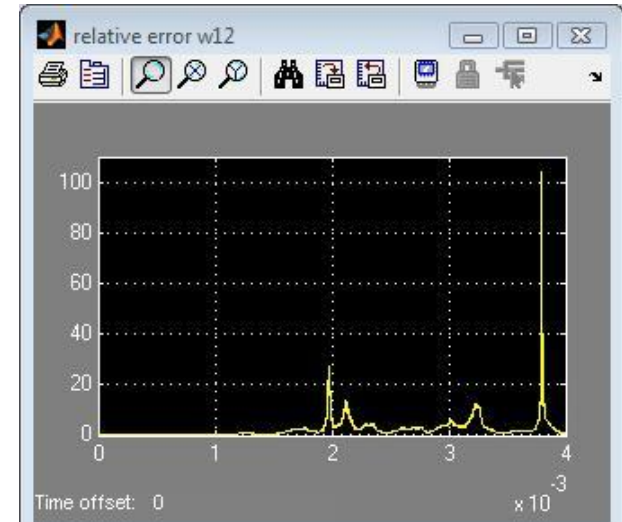
Limiting cases: if  $w_{12} = jw_{11}$  then  $\delta = 0$   
if  $w_{12} = -jw_{11}$  then  $\delta \rightarrow \infty$



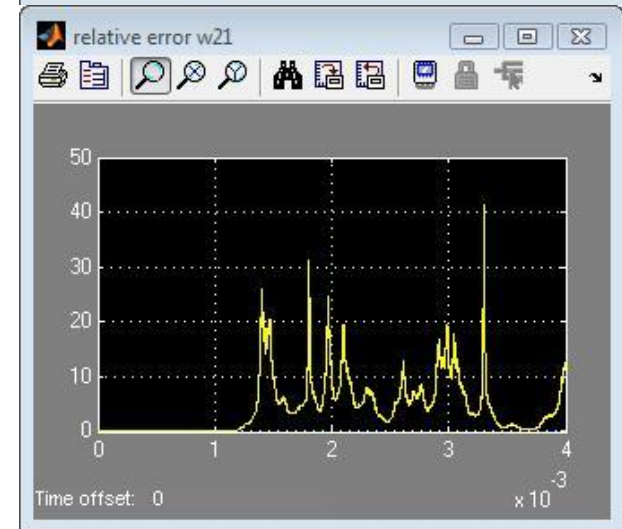
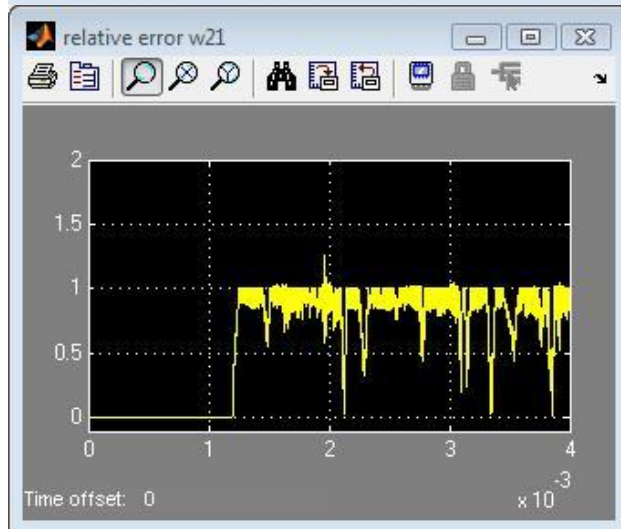
# COEFFICIENT RESTRICTION WITH MEASURED DATA



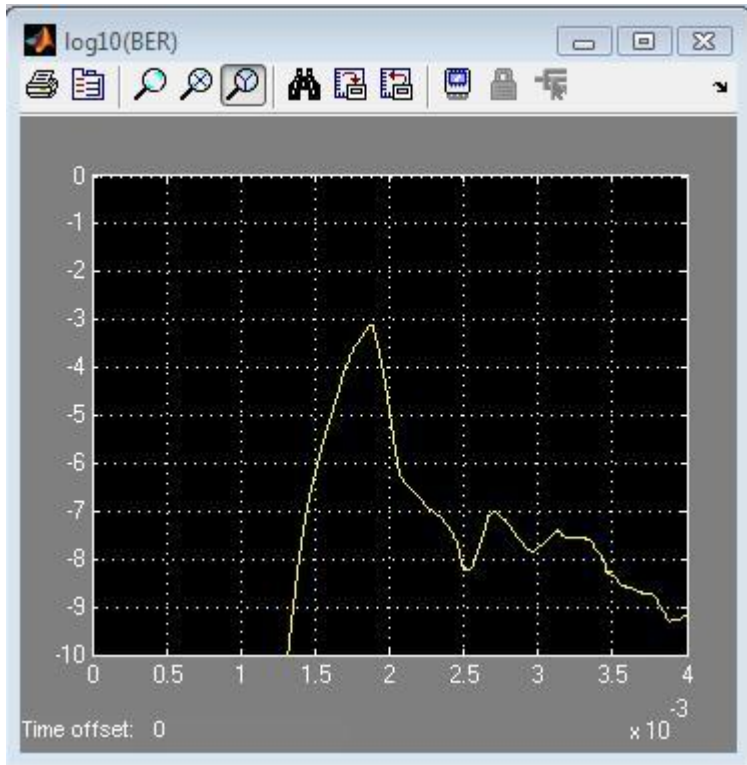
cancellation on



cancellation off



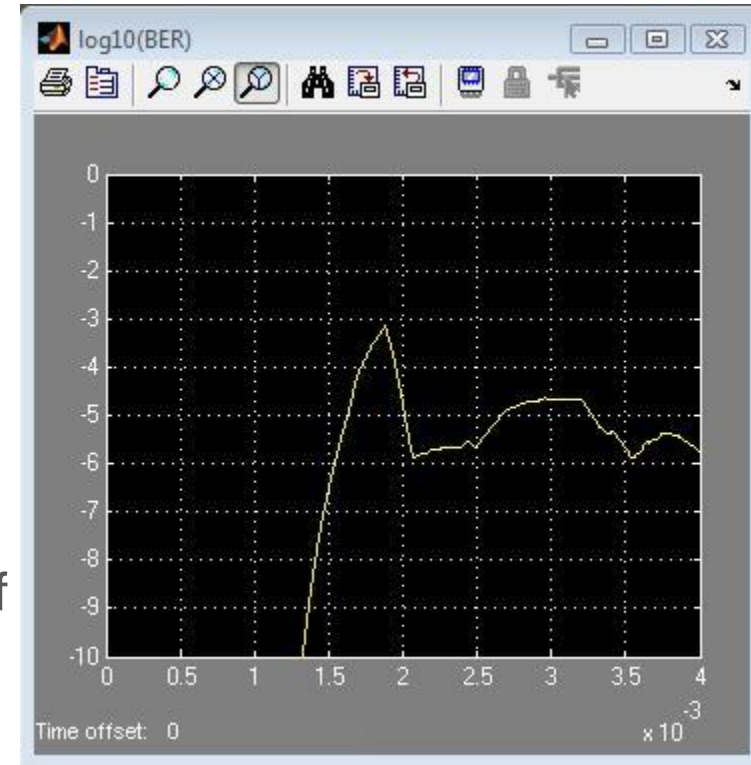
# BIT ERROR RATE, MEAS. NO. 4



cancellation on



cancellation off



# OBSERVATIONS

- › False detection cancellation does not necessarily result in worse bit error rate
- › If bit error rate is worse then it is still acceptable
- › Advantage: Much simpler than earlier ideas, fits better for FPGA realization
- › Still needs to be verified, improved

# CONCLUSIONS

- A **2x2 receiver** was shown based on **FFT approach**. All rotations were intended to be compensated before the equalizer
- In practice, not all rotations are compensated and rotated equalizer coefficients are required, resulting in false detection. To eliminate this effect, a **method for false detection cancellation** was shown

# KÖSZÖNET

Vámos Ábelnek és Dr. Verebély Pálnak, akik ezt a projectet lehetővé tették.

Q&A